

## 10. Autonomous Linear Dynamical Systems

- Linear dynamical systems
- Phase plane
- RLC circuits
- Chemical reactions
- Markov chains
- Higher-order linear systems
- Mechanical systems
- Linearization

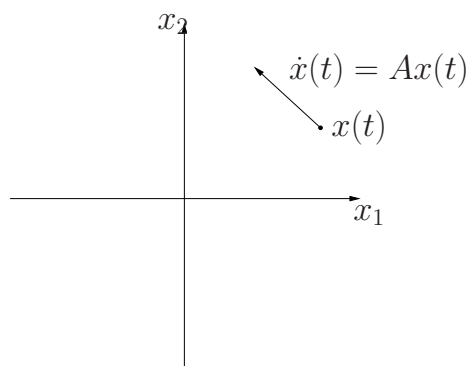
### Autonomous linear dynamical systems

continuous-time autonomous LDS has form

$$\dot{x} = Ax$$

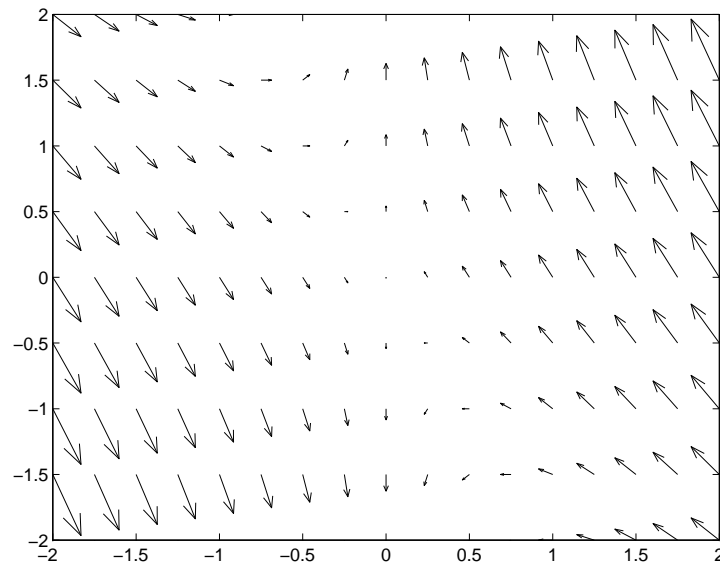
- $x(t) \in \mathbb{R}^n$  is called the state
- $n$  is the *state dimension* or (informally) the *number of states*
- $A$  is the *dynamics matrix*  
(system is *time-invariant* if  $A$  doesn't depend on  $t$ )

picture (*phase plane*):

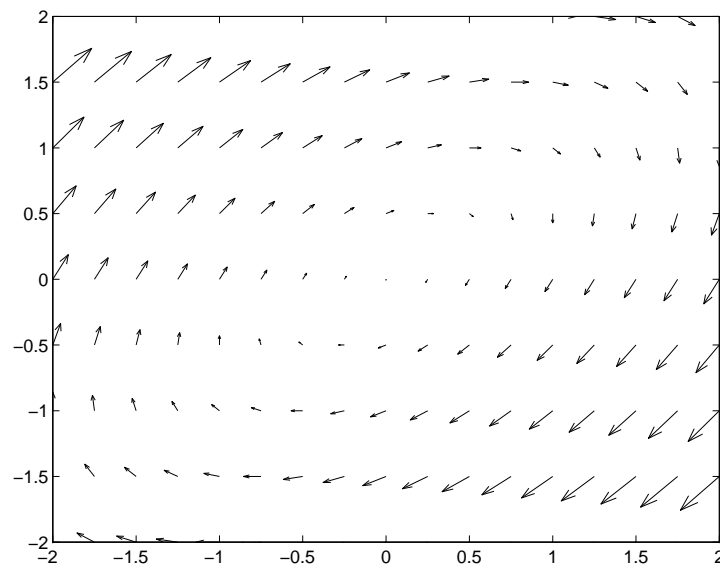


**Example 1: Autonomous linear dynamical systems**

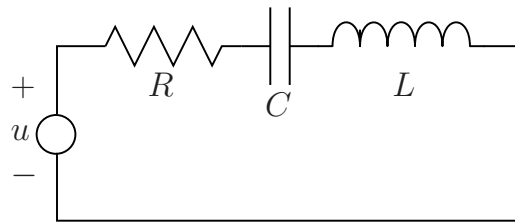
$$\dot{x} = \begin{bmatrix} -1 & 0 \\ 2 & 1 \end{bmatrix} x$$

**Example 2: Autonomous linear dynamical systems**

$$\dot{x} = \begin{bmatrix} -0.5 & 1 \\ -1 & 0.5 \end{bmatrix} x$$



## Linear circuit



Let  $x_1$  be the voltage across  $C$  and  $x_2$  be the current through  $L$ , then

$$\begin{aligned} u &= Rx_2 + x_1 + L\dot{x}_2 \\ x_2 &= C\dot{x}_1 \end{aligned}$$

and hence  $\dot{x} = Ax + Bu$  where

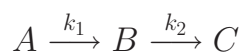
$$A = \begin{bmatrix} 0 & 1/C \\ -1/L & -R/L \end{bmatrix} \quad B = \begin{bmatrix} 0 \\ 1/L \end{bmatrix}$$

## Chemical reactions

- reaction involving  $n$  chemicals;  $x_i$  is concentration of chemical  $i$
- linear model of reaction kinetics

$$\frac{dx_i}{dt} = a_{i1}x_1 + \cdots + a_{in}x_n$$

**Example:** series reaction

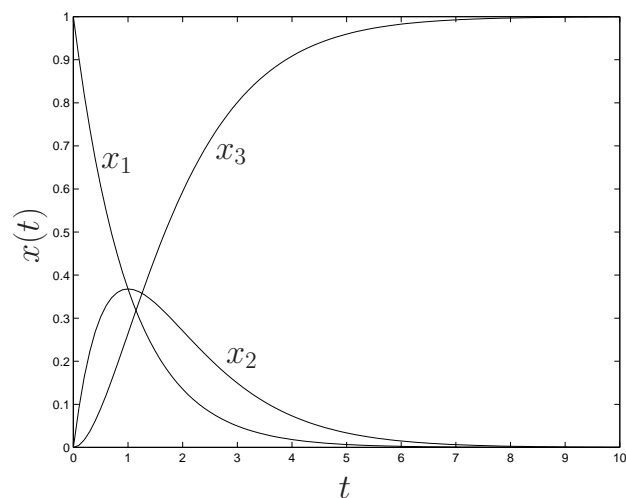


with linear dynamics

$$\dot{x} = \begin{bmatrix} -k_1 & 0 & 0 \\ k_1 & -k_2 & 0 \\ 0 & k_2 & 0 \end{bmatrix} x$$

plot for  $k_1 = k_2 = 1$

initial  $x(0) = (1, 0, 0)$



## Finite-state discrete-time Markov chain

$z(t) \in \{1, \dots, n\}$  is a random sequence with

$$\text{Prob}(z(t+1) = i \mid z(t) = j) = P_{ij}$$

where  $P \in \mathbb{R}^{n \times n}$  is the matrix of *transition probabilities*

represent probability distribution of  $z(t)$  as  $n$ -vector

$$p(t) = \begin{bmatrix} \text{Prob}(z(t) = 1) \\ \vdots \\ \text{Prob}(z(t) = n) \end{bmatrix}$$

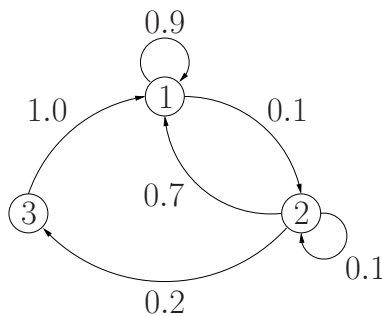
then

$$p(t+1) = Pp(t)$$

## Example: Finite-state Markov chain

Markov chain is depicted graphically

- nodes are states
- edges show transition probabilities



- state 1 is 'system OK'
- state 2 is 'system down'
- state 3 is 'system being repaired'

$$p(t+1) = \begin{bmatrix} 0.9 & 0.7 & 1.0 \\ 0.1 & 0.1 & 0 \\ 0 & 0.2 & 0 \end{bmatrix} p(t)$$

## Higher order linear dynamical systems

$$x^{(k)} = A_{k-1}x^{(k-1)} + \dots + A_1x^{(1)} + A_0x, \quad x(t) \in \mathbb{R}^n$$

where  $x^{(m)}$  denotes  $m$ th derivative

define new variable  $z = \begin{bmatrix} x \\ x^{(1)} \\ \vdots \\ x^{(k-1)} \end{bmatrix} \in \mathbb{R}^{nk}$ , so

$$\dot{z} = \begin{bmatrix} x^{(1)} \\ \vdots \\ x^{(k)} \end{bmatrix} = \begin{bmatrix} 0 & I & 0 & \dots & 0 \\ 0 & 0 & I & \dots & 0 \\ \vdots & & & & \vdots \\ 0 & 0 & 0 & \dots & I \\ A_0 & A_1 & A_2 & \dots & A_{k-1} \end{bmatrix} z$$

a (first order) LDS (with bigger state)

## Mechanical systems

mechanical system with  $k$  degrees of freedom undergoing small motions:

$$M\ddot{q} + D\dot{q} + Kq = 0$$

- $q(t) \in \mathbb{R}^k$  is the vector of generalized displacements
- $M$  is the *mass matrix*
- $K$  is the *stiffness matrix*
- $D$  is the *damping matrix*

with state  $x = \begin{bmatrix} q \\ \dot{q} \end{bmatrix}$  we have

$$\dot{x} = \begin{bmatrix} \dot{q} \\ \ddot{q} \end{bmatrix} = \begin{bmatrix} 0 & I \\ -M^{-1}K & -M^{-1}D \end{bmatrix} x$$

## Linearization near equilibrium point

nonlinear, time-invariant differential equation (DE):

$$\dot{x} = f(x)$$

where  $f : \mathbb{R}^n \rightarrow \mathbb{R}^n$

suppose  $x_e$  is an *equilibrium point*, i.e.,  $f(x_e) = 0$   
(so  $x(t) = x_e$  satisfies DE)

now suppose  $x(t)$  is near  $x_e$ , so

$$\dot{x}(t) = f(x(t)) \approx f(x_e) + Df(x_e)(x(t) - x_e)$$

with  $\delta x(t) = x(t) - x_e$ , rewrite as

$$\dot{\delta x}(t) \approx Df(x_e)\delta x(t)$$

replacing  $\approx$  with  $=$  yields *linearized approximation* of DE near  $x_e$

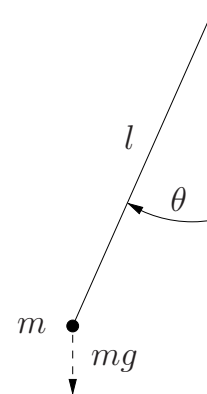
we *hope* solution of  $\dot{\delta x} = Df(x_e)\delta x$  is a good approximation of  $x - x_e$

## Example: pendulum

2nd order nonlinear DE  $m l^2 \ddot{\theta} = -l m g \sin \theta$

rewrite as first order DE with state  $x = \begin{bmatrix} \theta \\ \dot{\theta} \end{bmatrix}$ :

$$\dot{x} = \begin{bmatrix} x_2 \\ -(g/l) \sin x_1 \end{bmatrix}$$



equilibrium point (pendulum down):  $x = 0$

linearized system near  $x_e = 0$ :

$$\dot{\delta x} = \begin{bmatrix} 0 & 1 \\ -g/l & 0 \end{bmatrix} \delta x$$

## Does linearization 'work'?

the linearized system usually, but not always, gives a good idea of the system behavior near  $x_e$

**example 1:**  $\dot{x} = -x^3$  near  $x_e = 0$

for  $x(0) > 0$  solutions have form  $x(t) = (x(0)^{-2} + 2t)^{-1/2}$

linearized system is  $\dot{\delta x} = 0$ ; solutions are constant

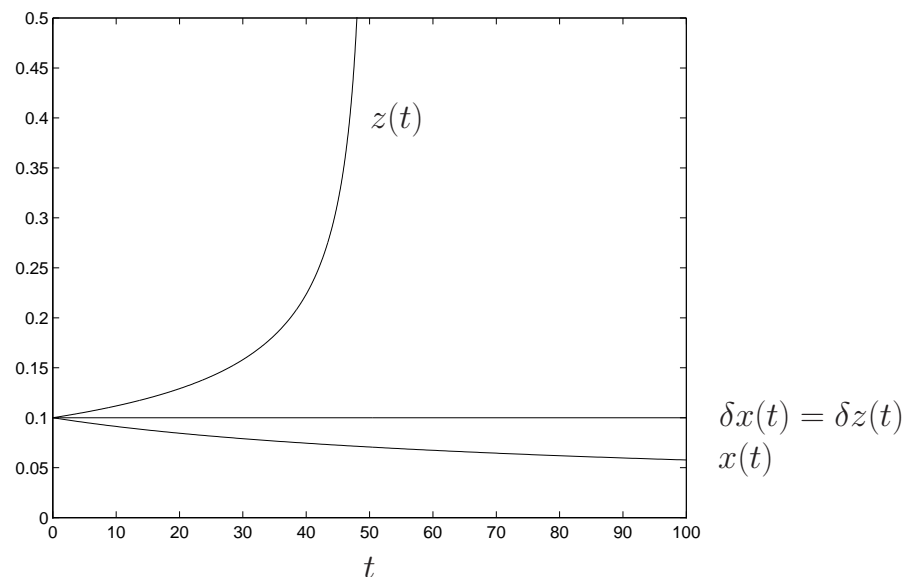
**example 2:**  $\dot{z} = z^3$  near  $z_e = 0$

for  $z(0) > 0$  solutions have form  $z(t) = (z(0)^{-2} - 2t)^{-1/2}$

(finite escape time at  $t = z(0)^{-2}/2$ )

linearized system is  $\dot{\delta z} = 0$ ; solutions are constant

## Does linearization 'work'?



- systems with very different behavior have same linearized system
- linearized systems do not predict qualitative behavior of either system